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Polarization imaging of multiply-scattered radiation based on Integral-Vector Monte Carlo Method

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Contents

- ✘ Introduction
 - Context
 - Objectives
- ✘ Modeling
 - Formalism
 - Problem definition
 - Integral formulation of the VRTE with a SOSS
 - Monte Carlo integration
- ✘ Polarization imaging application
 - Backscattering configuration (validation)
 - Lateral configuration
 - Sensitivity to morphology
 - Experimentation
- ✘ Conclusion/ Expectations

Context

Size & structure characterization of complex-shaped particles in semi-transparent media



**Non intrusive techniques → Electromagnetic waves (light)
Intensity + polarization (Stokes formalism, Mueller matrix)**

Existing applications

◦ **Optically thin media** ◦
→ **single scattering regime**

in-between

◦◦ **Optically thick media** ◦◦
→ **Diffusion approximation**

multiple scattering effects



**To increase information: 2D distribution = imaging
Polarization pattern = signature of the medium**


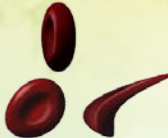

Objectives

2D Optical diagnostic of semi transparent heterogeneous media
analyzing polarization state with the Stokes parameter formalism

Characterization of :

- ✦ Optical / Radiative properties
- ✦ Morphology
- ✦ Size dispersion
- ✦ Volumetric fraction

Examples of a large scope of applications

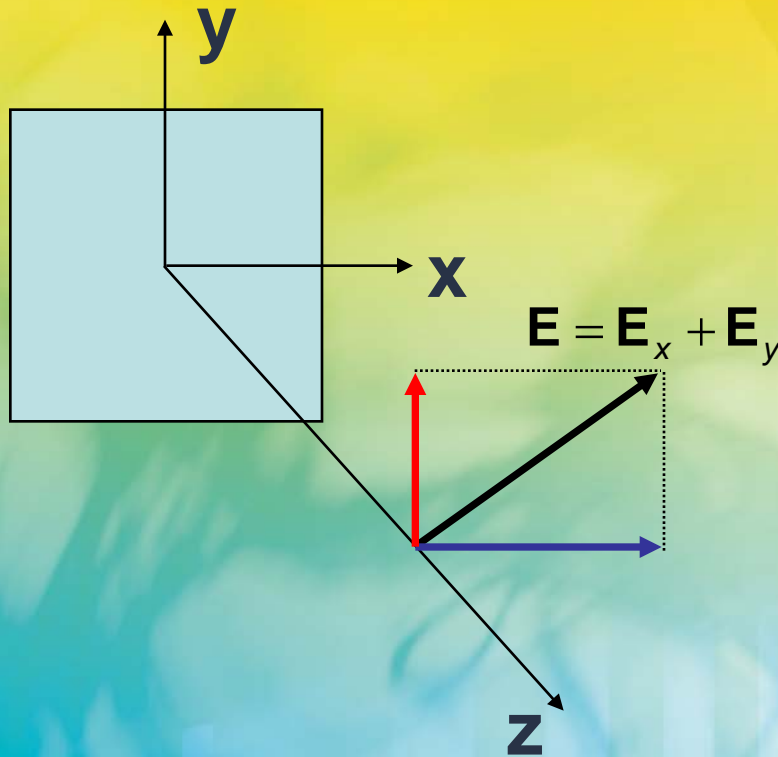
- ✦ Particle suspensions, soot 
- ✦ Biological cells 
- ✦ Circumstellar disks 

Polarization pattern from multiple scattering effects
→ need of comprehensive models

Modeling polarization imaging in a 3D system:
Integral-Vector Monte Carlo Method

Formalism – Polarization

Plane harmonic wave propagating in homogeneous medium



$$\mathbf{E}_x(z, t) = E_{0x} \cos(kz - \omega t) \mathbf{x}$$

$$\mathbf{E}_y(z, t) = E_{0y} \cos(kz - \omega t - \delta) \mathbf{y}$$

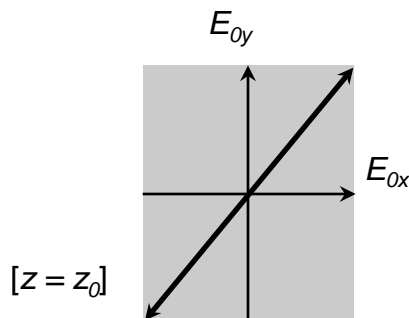
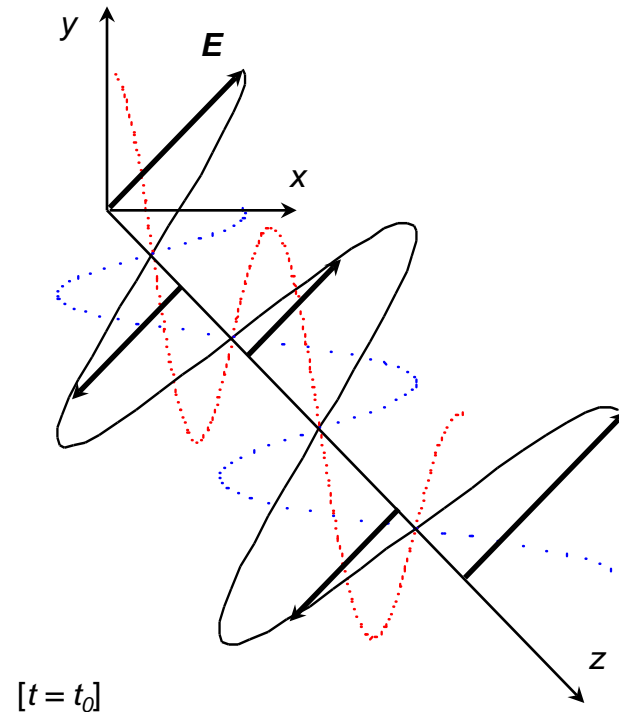
ω : angular frequency

k : wave vector

E_{0x}, E_{0y} : component amplitudes

δ : phase difference between components

Formalism – Polarization



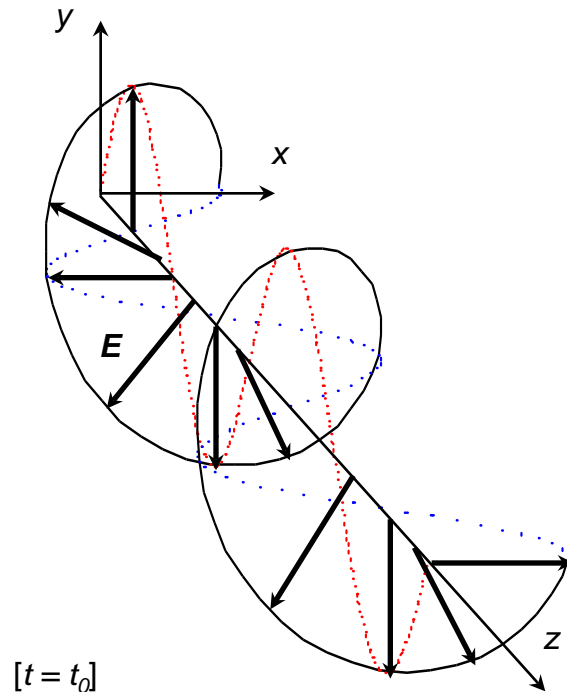
If $\delta = 0 [2\pi]$

$$\mathbf{E}(z, t) = (E_{0x} \mathbf{x} + E_{0y} \mathbf{y}) \cos(kz - \omega t)$$

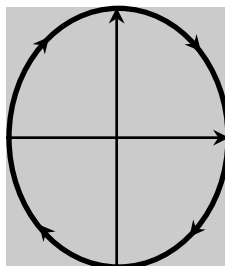
constant orientation of \mathbf{E}
(time independent)

linear polarization

Formalism – Polarization



$$E_{0y} = E_0$$



$$[z = z_0]$$

$$E_{0x} = E_0$$

$$\text{If } \delta = \pi/2 [2\pi]$$

$$E_{0x} = E_{0y} = E_0$$

$$\mathbf{E}_x(z, t) = E_0 \cos(kz - \omega t) \mathbf{x}$$

$$\begin{aligned} \mathbf{E}_y(z, t) &= E_0 \cos(kz - \omega t - \pi/2) \mathbf{y} \\ &= E_0 \sin(kz - \omega t) \mathbf{y} \end{aligned}$$

$$\mathbf{E}(z, t) = E_0 [\cos(kz - \omega t) \mathbf{x} + \sin(kz - \omega t) \mathbf{y}]$$

constant module of \mathbf{E} (E_0)

end of \mathbf{E} (in transverse plane) describes a circle

right circular polarization

Formalism – Stokes vector & Mueller matrix

- ✗ General case: Polarization state → elliptic polarization → ellipsometry
- ✗ How to describe polarization state of light with measurable quantities?
→ **Stokes vector**

$$\mathbf{I} = \begin{pmatrix} I \\ Q \\ U \\ V \end{pmatrix} = \begin{pmatrix} E_x \overline{E_x} + E_y \overline{E_y} \\ E_x \overline{E_x} - E_y \overline{E_y} \\ E_x \overline{E_y} + E_y \overline{E_x} \\ i(E_x \overline{E_y} - E_y \overline{E_x}) \end{pmatrix}$$

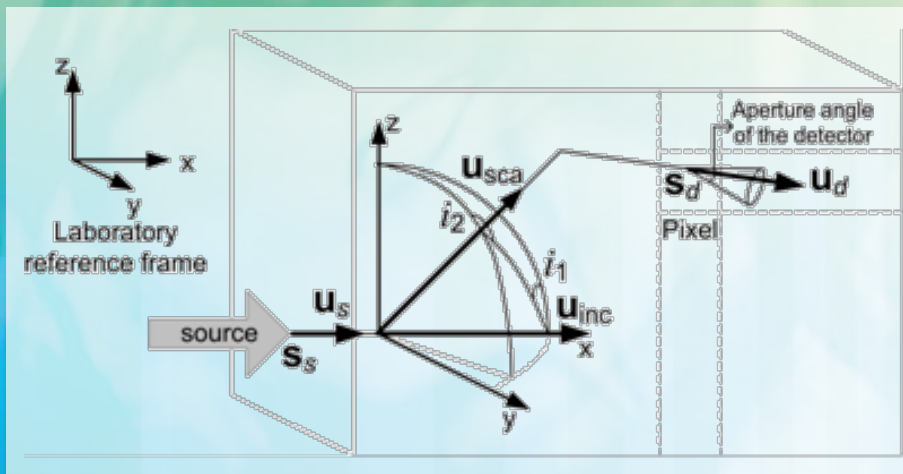
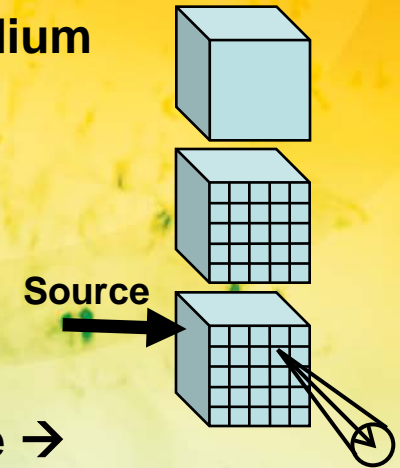
Information about
Intensity
Linear polarization (horizontal / vertical)
Linear polarization (oblique: +/- 45°)
Circular polarization (right / left)

- ✗ Relation between a Stokes vector source and a detected Stokes vector
→ effective **Mueller matrix**

$$\begin{pmatrix} I \\ Q \\ U \\ V \end{pmatrix}_{\text{detected}} = \begin{pmatrix} M_{11} & M_{12} & M_{13} & M_{14} \\ M_{21} & M_{22} & M_{23} & M_{24} \\ M_{31} & M_{32} & M_{33} & M_{34} \\ M_{41} & M_{42} & M_{43} & M_{44} \end{pmatrix} \begin{pmatrix} I \\ Q \\ U \\ V \end{pmatrix}_{\text{source}}$$

Problem definition

- ✗ System = Scattering, absorbing, non emitting cold medium
- ✗ Data = 2D distribution of M_{ij} on a defined surface in the space surrounding the system \rightarrow subdivision in pixels
- ✗ Detection within a given solid angle
- ✗ External radiation source
- ✗ Laboratory frame to keep track of the polarization state \rightarrow definition of the meridian plan containing the direction of propagation under consideration



$$\mathbf{I}_{sca} = \frac{\sigma}{4\pi} \mathbf{L}(\pi - i_2) \mathbf{S} \mathbf{L}(-i_1) \mathbf{I}_{inc} = \frac{\sigma}{4\pi} \mathbf{S}_R \mathbf{I}_{inc}$$

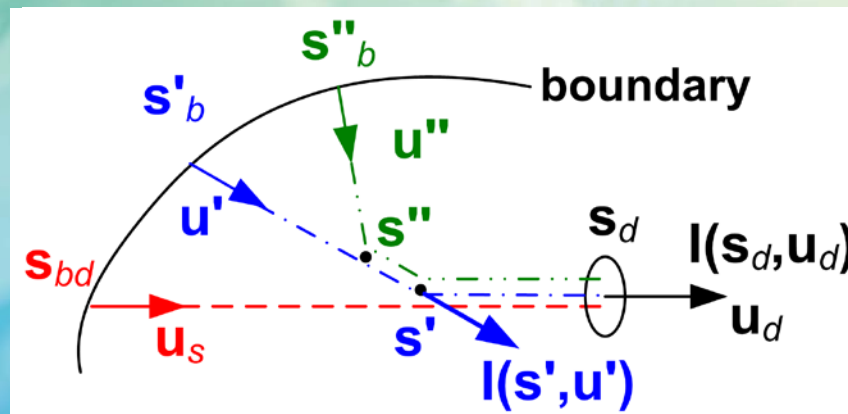
Integral formulation of the VRTE with a SOSS

The Vector Radiative Transfer Equation (VRTE)

Detected Stokes vector $\mathbf{I}(\mathbf{s}_d, \mathbf{u}_d)$ = Transmittance $\mathbf{I}(\mathbf{s}_{bd}, \mathbf{u}_d) t(\mathbf{s}_{bd}, \mathbf{s}_d)$ + Scattering coefficient $\int_{\mathbf{s}_{bd}}^{\mathbf{s}_d} ds' t(\mathbf{s}', \mathbf{s}_d) \frac{\sigma}{4\pi} \int_{4\pi} du' \mathbf{S}_R(\mathbf{s}', \mathbf{u}', \mathbf{u}_d) \mathbf{I}(\mathbf{s}', \mathbf{u}')$ Rotated scattering matrix

Position \mathbf{s}_d Direction \mathbf{u}_d

$$\mathbf{I}(\mathbf{s}_d, \mathbf{u}_d) = \mathbf{I}(\mathbf{s}_{bd}, \mathbf{u}_d) t(\mathbf{s}_{bd}, \mathbf{s}_d) + \int_{\mathbf{s}_{bd}}^{\mathbf{s}_d} ds' t(\mathbf{s}', \mathbf{s}_d) \frac{\sigma}{4\pi} \int_{4\pi} du' \mathbf{S}_R(\mathbf{s}', \mathbf{u}', \mathbf{u}_d) \left\{ \mathbf{I}(\mathbf{s}'_b, \mathbf{u}') t(\mathbf{s}'_b, \mathbf{s}') + \int_{\mathbf{s}'_b}^{\mathbf{s}'_d} ds'' t(\mathbf{s}'', \mathbf{s}') \frac{\sigma}{4\pi} \int_{4\pi} du'' \mathbf{S}_R(\mathbf{s}'', \mathbf{u}'', \mathbf{u}') \mathbf{I}(\mathbf{s}'', \mathbf{u}'') \right\}$$



Integral formulation of the VRTE with a SOSS

The Scattering Order of Scattering Series (SOSS)

$$\overset{\text{Detected Stokes vector}}{\mathbf{I}(s_d, \mathbf{u}_d)} = \sum_{k=0}^{\infty} \overset{\text{Scattering orders}}{\mathbf{I}_k}$$

\mathbf{I}_k is the k^{th} scattering order Stokes vector
viz. the ensemble of contributions which are considered with k scattering modifications of propagation direction between a source and the detector

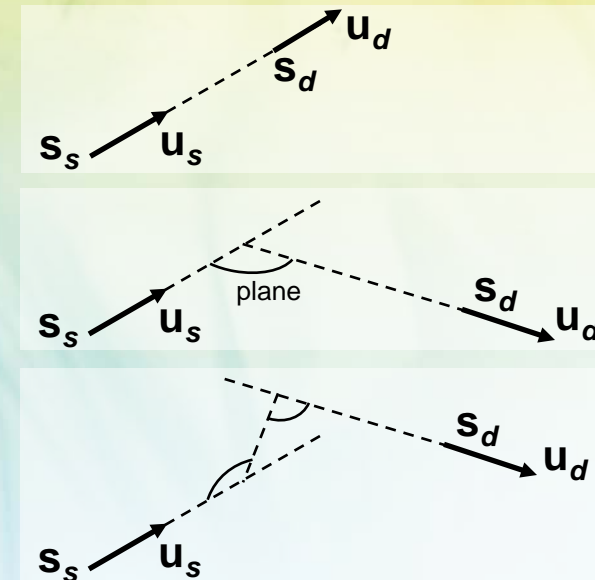
$\mathbf{I}_0 \neq 0$ only if a source is aligned with the detector

$$\mathbf{I}_0(s_d, \mathbf{u}_d) = \mathbf{I}(s_s, \mathbf{u}_s) t(s_s, s_d)$$

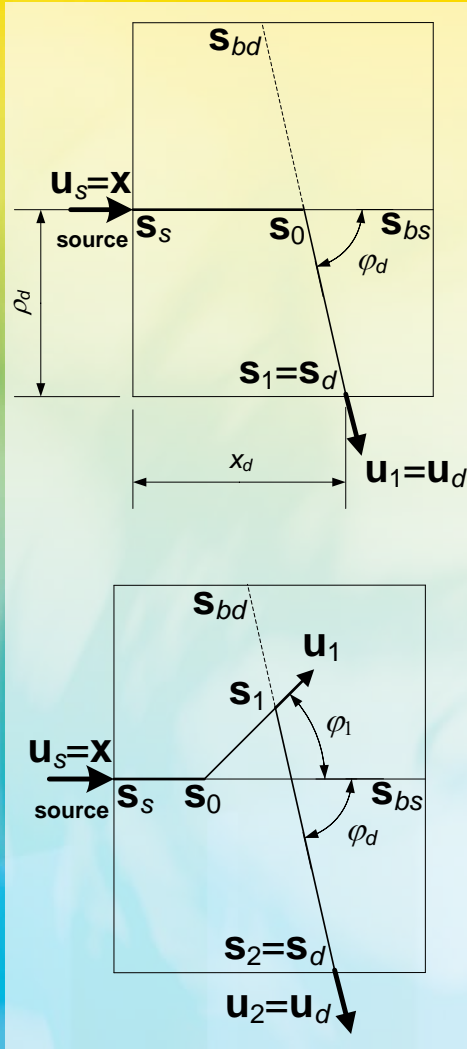
$\mathbf{I}_1 \neq 0$ only if a source and the detector directions ($\mathbf{u}_s, \mathbf{u}_d$) are in the same plane

General 3D case

at least two modifications of propagation direction are necessary to reach the detector from the source,
viz. $\mathbf{I}_0 = \mathbf{I}_1 = 0$



Integral formulation of the VRTE with a SOSS



First scattering orders in a uniform media

$$I_1(\mathbf{s}_d, \mathbf{u}_d) = \frac{\omega}{4\pi\rho_d \sin \varphi_d} \exp\left(-\beta\left(x_d + \rho_d \tan\left(\frac{\varphi_d}{2}\right)\right)\right) S_R(\mathbf{u}_d, \mathbf{x}) I(\mathbf{s}_s, \mathbf{x})$$

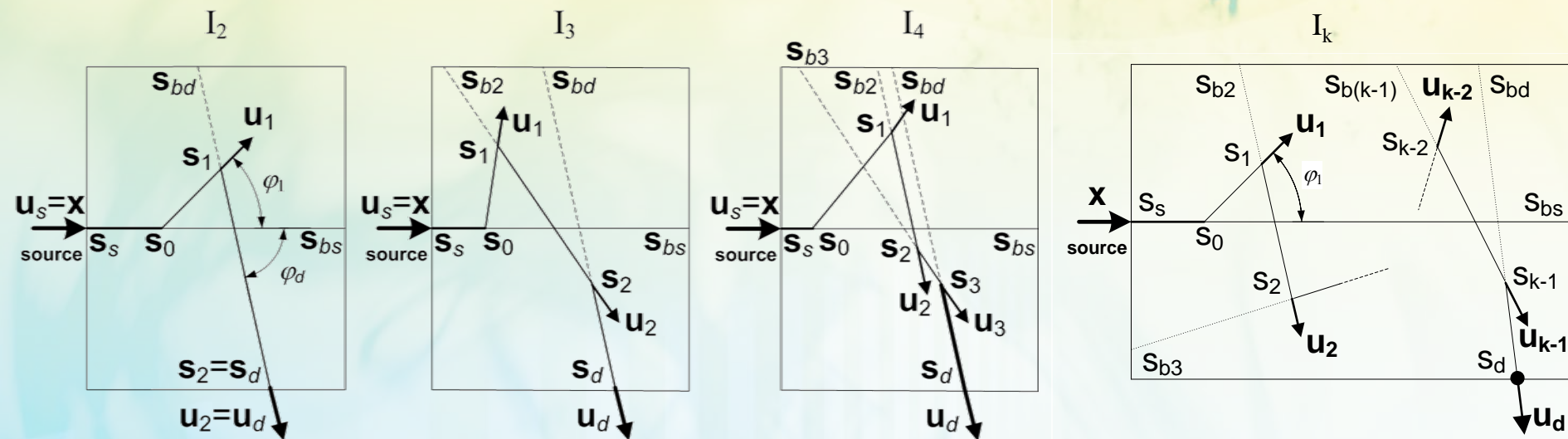
Albedo ω
 Extinction coefficient β
 Scattering angle φ_d
 Position and direction of the source $(\mathbf{s}_s, \mathbf{x})$
 distance from \mathbf{x} axis x_d
 distance from the source on \mathbf{x} axis ρ_d

$$I_2(\mathbf{s}_2, \mathbf{u}_2) = \int_{s_{b2}}^{s_2} \int_{s_{bs}}^{s_s} \left(\frac{\omega}{4\pi}\right)^2 \frac{t(\mathbf{s}_s, \mathbf{s}_0)t(\mathbf{s}_0, \mathbf{s}_1)t(\mathbf{s}_1, \mathbf{s}_2)}{\|\mathbf{s}_1 - \mathbf{s}_0\|^2} S_R(\mathbf{u}_2, \mathbf{u}_1) S_R(\mathbf{u}_1, \mathbf{x}) I(\mathbf{s}_s, \mathbf{x}) ds_0 ds_1$$

Integral formulation of the VRTE with a SOSS

✗ Recursive formulation for higher orders

$$\mathbf{I}_k(\mathbf{s}_d, \mathbf{u}_d) = \frac{\omega}{4\pi} \int_{s_{bd}}^{s_d} \int_0^{2\pi} \int_{-1}^1 t(\mathbf{s}_{k-1}, \mathbf{s}_d) \mathbf{S}_R(\mathbf{u}_d, \mathbf{u}_{k-1}) \mathbf{I}_{k-1}(\mathbf{s}_{k-1}, \mathbf{u}_{k-1}) d\eta_{k-1} d\psi_{k-1} ds_{k-1}$$



✗ These integrals cannot be solved analytically for complex geometries

Monte Carlo integration

✘ Principle

$$\int_D f(x) dx = \int_D \overset{\substack{\text{Probability density function} \\ \text{of a random variable } X}}{\text{pdf}_X(x)} \frac{f(x)}{\text{pdf}_X(x)} dx = \int_D \text{pdf}_X(x) w(x) dx = \lim_{N \rightarrow \infty} m, \overset{\text{Estimation}}{m} = \frac{1}{N} \sum_{i=1}^N w(x_i)$$

ROGER, M., BLANCO, S., EL HAFI, M., FOURNIER, R., Monte Carlo Estimates of Domain-Deformation Sensitivities, *Phys. Rev. Lett.*, volume 95, issue 18, pages 180601.1-4, 2005

- Judicious choices for **probability density functions (pdf)**

+

- Computation of the series is a **backward** process:
a priori better adapted to **directional detection** than a forward process

→ **Efficient reduction of variance**

MC Integration → sampling integration domains thanks to appropriate chosen pdfs

Monte Carlo integration

✘ Implementation

● Variance and accuracy control (sample variance)

$$\text{var}_m = \frac{1}{N} \left(\frac{1}{N} \sum_{i=1}^N w(x_i)^2 - \left(\frac{1}{N} \sum_{i=1}^N w(x_i) \right)^2 \right), \text{var}_{sp} = \frac{N_{sp}}{N_{sp} - 1} \left(\frac{1}{N_{sp}} \sum_{i=1}^{N_{sp}} m_i^2 - \left(\frac{1}{N_{sp}} \sum_{i=1}^{N_{sp}} m_i \right)^2 \right)$$

● MC Formulation

$$\mathbf{I}_k(\mathbf{s}_d, \mathbf{u}_d) = \frac{\omega}{4\pi} \int_{s_{bd}}^{s_d} \int_0^{2\pi} \int_{-1}^1 t(\mathbf{s}_{k-1}, \mathbf{s}_d) \mathbf{S}_R(\mathbf{u}_d, \mathbf{u}_{k-1}) \mathbf{I}_{k-1}(\mathbf{s}_{k-1}, \mathbf{u}_{k-1}) d\eta_{k-1} d\psi_{k-1} ds_{k-1}$$

- pdf choice → cumulative density function (cdf) → variable change

$$R_{s_{k-1}} = \frac{1 - t(\mathbf{s}_{k-1}, \mathbf{s}_d)}{1 - t(\mathbf{s}_{bd}, \mathbf{s}_d)}, R_{\psi_{k-1}} = \frac{\psi_{k-1}}{2\pi}, dR_{\eta_{k-1}} = \frac{\mathbf{S}_{R11}(\mathbf{u}_d, \mathbf{u}_{k-1})}{2} d\eta_{k-1}$$

$$\mathbf{I}_k(\mathbf{s}_d, \mathbf{u}_d) = \omega (1 - t(\mathbf{s}_{bd}, \mathbf{s}_d)) \int_0^1 \int_0^1 \int_0^1 \frac{\mathbf{S}_R(\mathbf{u}_d, \mathbf{u}_{k-1})}{\mathbf{S}_{R11}(\mathbf{u}_d, \mathbf{u}_{k-1})} \mathbf{I}_{k-1}(\mathbf{s}_{k-1}, \mathbf{u}_{k-1}) dR_{\eta_{k-1}} dR_{\psi_{k-1}} dR_{s_{k-1}}$$

Backscattering configuration (validation)

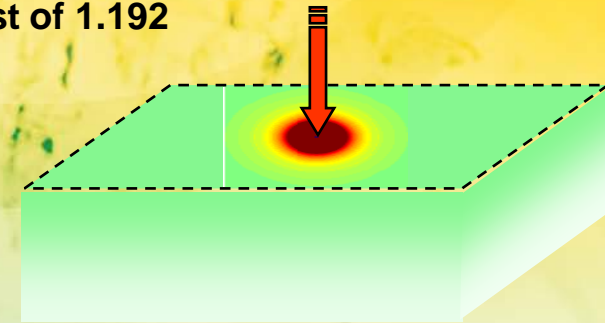
- i. against the semi-analytical results of Crosbie and Dougherty (1982) for **scalar backscattered intensities** in the case of a plane parallel layer of **isotropic scattering** media subjected to a Gaussian narrow beam

- ii. against Ambirajan and Look (1997) results for the **backscattered Stokes vector** intensities calculated as a function of the distance of observation from a right circularly polarized narrow beam illuminating a plane-parallel medium laden with **spherical particles**

Backscattering configuration (validation)

Rakovic et al (1999)

2D effective Mueller matrix contours from a half-space filled with a suspension of monodispersed spheres with a size parameter $x=13.4$ and a refractive index contrast of 1.192


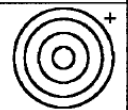

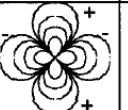
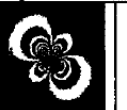
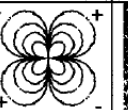
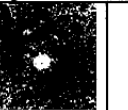


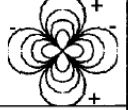

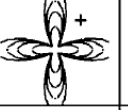
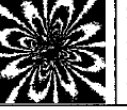
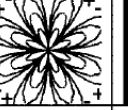
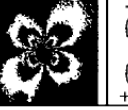
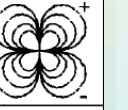

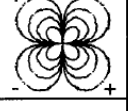











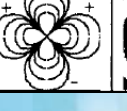




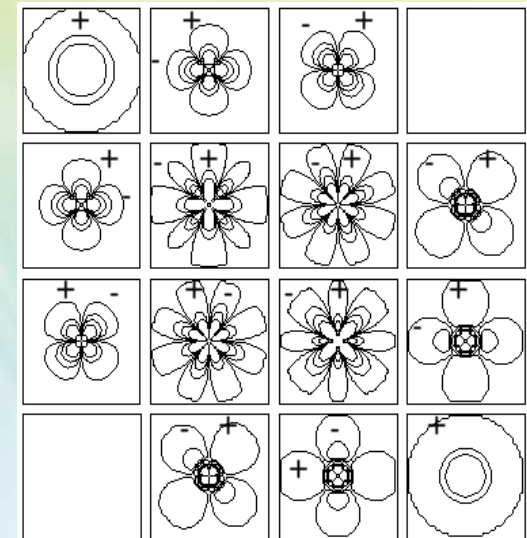
$$\begin{matrix} M_{11} & M_{12} & M_{13} & M_{14} \\ M_{21} & M_{22} & M_{23} & M_{24} \\ M_{31} & M_{32} & M_{33} & M_{34} \\ M_{41} & M_{42} & M_{43} & M_{44} \end{matrix}$$

$$\begin{matrix} M_{21} & M_{22} & M_{23} & M_{24} \\ M_{31} & M_{32} & M_{33} & M_{34} \\ M_{41} & M_{42} & M_{43} & M_{44} \end{matrix}$$

$$\begin{matrix} M_{31} & M_{32} & M_{33} & M_{34} \\ M_{41} & M_{42} & M_{43} & M_{44} \end{matrix}$$

$$\begin{matrix} M_{41} & M_{42} & M_{43} & M_{44} \end{matrix}$$

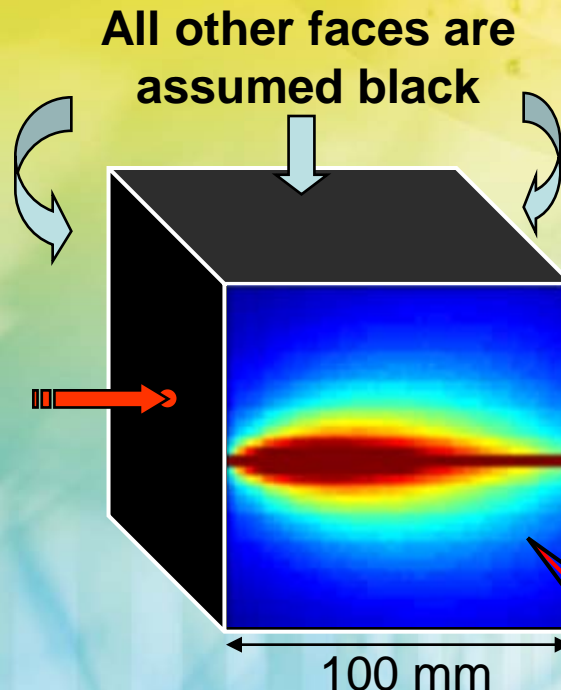
$S_{11}=(OO)$		$S_{12}=(HO-VO)$		$S_{13}=(PO-MO)$		$S_{14}=(RO-LO)$	
Experimental	Monte Carlo	Experimental	Monte Carlo	Experimental	Monte Carlo	Experimental	Monte Carlo
							
$S_{21}=(OH-OV)$		$S_{22}=(HH+VV)-(HV+VH)$		$S_{23}=(PH+MV)-(PV+MH)$		$S_{24}=(RH+LV)-(RV+LH)$	
							
$S_{31}=(OP-OM)$		$S_{32}=(HP+VM)-(HM+VP)$		$S_{33}=(PP+MM)-(PM+MP)$		$S_{34}=(RP+LM)-(RM+LP)$	
							
$S_{41}=(OR-OL)$		$S_{42}=(HR+VL)-(HL+VR)$		$S_{43}=(PR+ML)-(PL+MR)$		$S_{44}=(RR+LL)-(RL+LR)$	
							



Lateral configuration

Effective Mueller matrix images of a uniform non absorbing particle-laden solution

Polarized
monochromatic source
collimated at the center
2D Gaussian shape
optical FWHM of $1 \cdot 10^{-3}$
(narrow)
 $\lambda = 0.633 \mu\text{m}$



All other faces are
assumed black

100 mm

The refractive index ratio
 $n_{\text{particles}} / n_{\text{surrounding medium}} = 1.195$
(polystyrene particles in water
at $\lambda = 0.633 \mu\text{m}$)

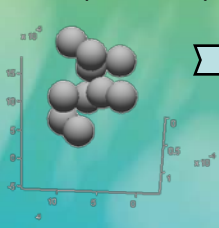
normal detection direction
within a conical aperture of 2°

Sensitivity to morphology

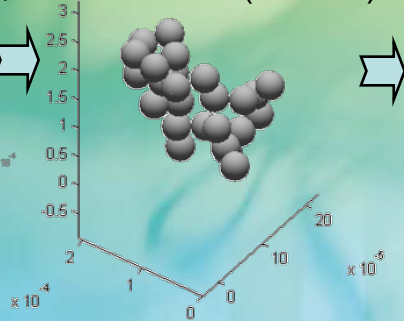
“Aggregation”

- ✗ Random generation
- ✗ Fractal dimension $D_f = 1.8$
- ✗ Prefactor $k_f = 2$
- ✗ Monomer diameter : 40 nm
- ✗ Constant volume fraction, $f_v = 2.E-4$

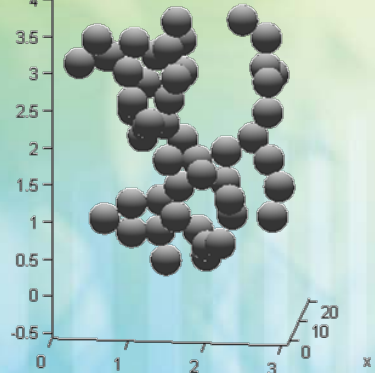
N10 ($x=0.57$)



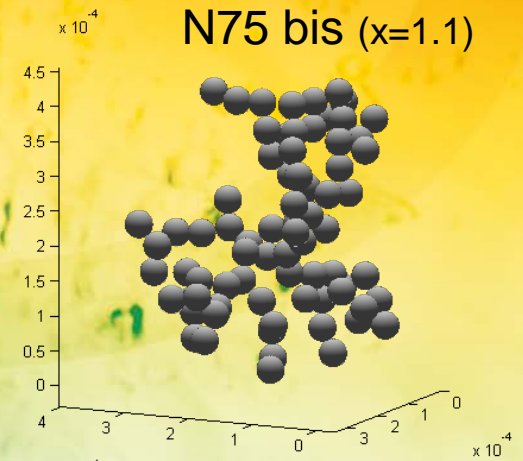
N25 ($x=0.77$)



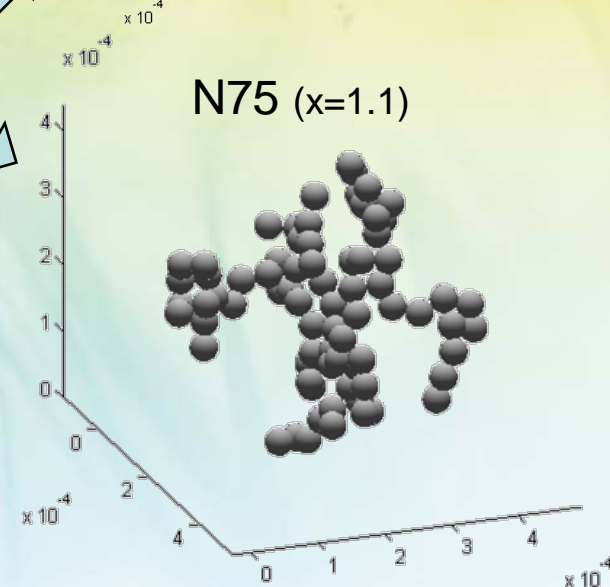
N50 ($x=0.97$)



N75 bis ($x=1.1$)

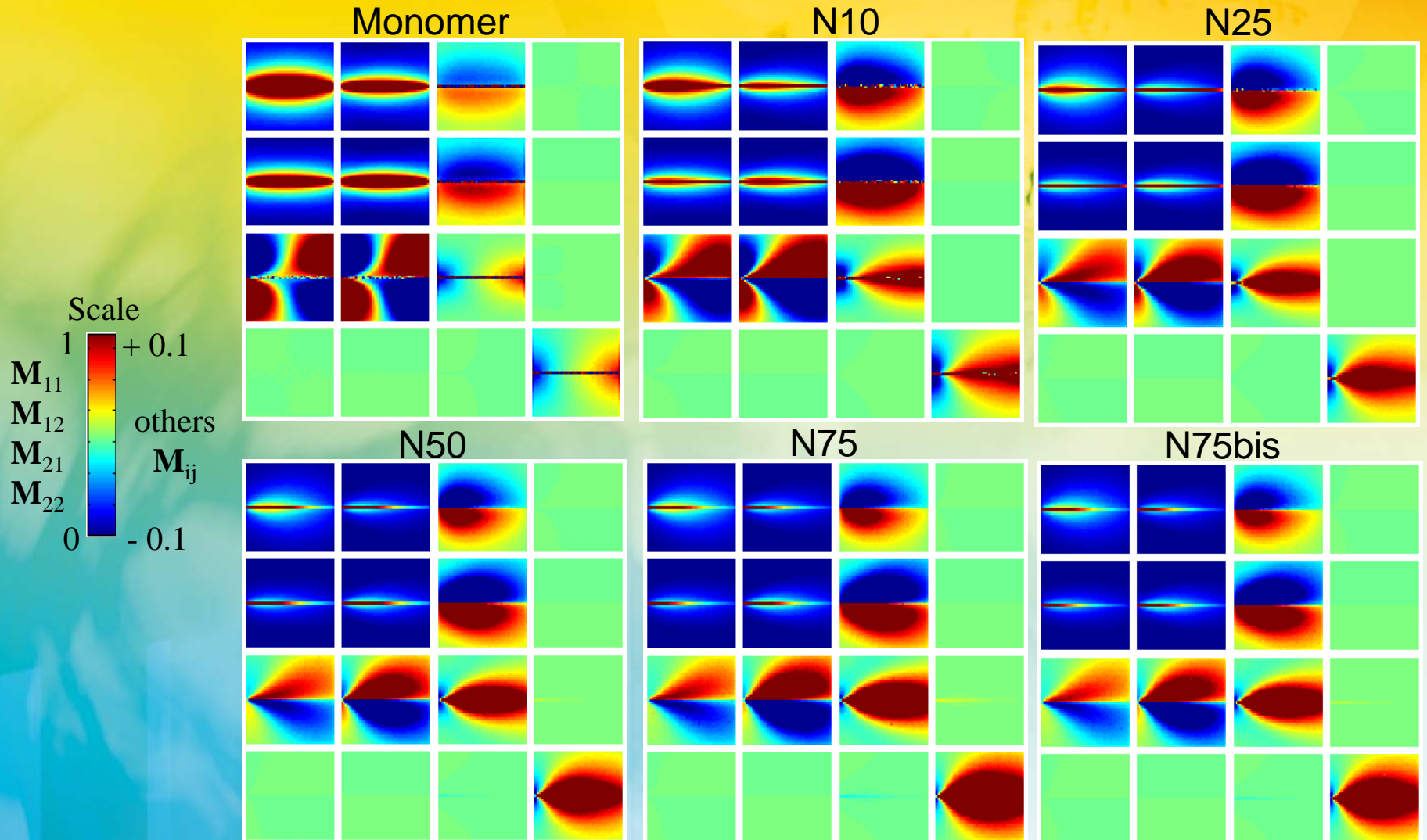


N75 ($x=1.1$)



Agg	Mono	N10	N25	N50	N75	N75bis
σ (m^{-1})	3.822	11.87	20.93	26.87	27.30	29.02

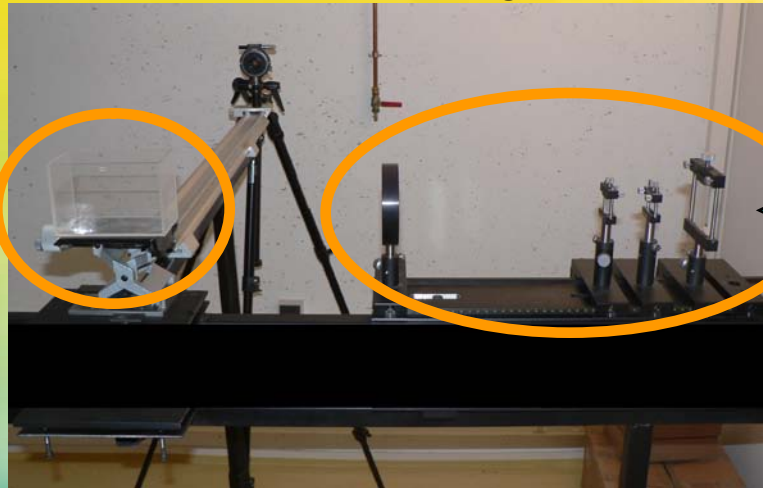
Sensitivity to morphology



Experimental setup

- ✘ Measure of Stokes parameters $\mathbf{I} = (I \ Q \ U \ V)^t$, on each pixel of different pictures, at 90° , in a small solid angle

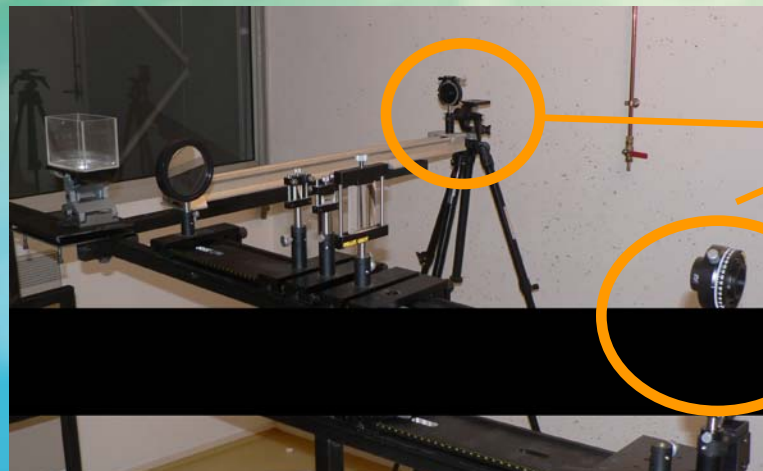
Sample



Shaping the polarized
collimated laser sheet

$$458 < \lambda < 514 \text{ nm}$$

$$1 < \text{Power} < 4 \text{ W}$$



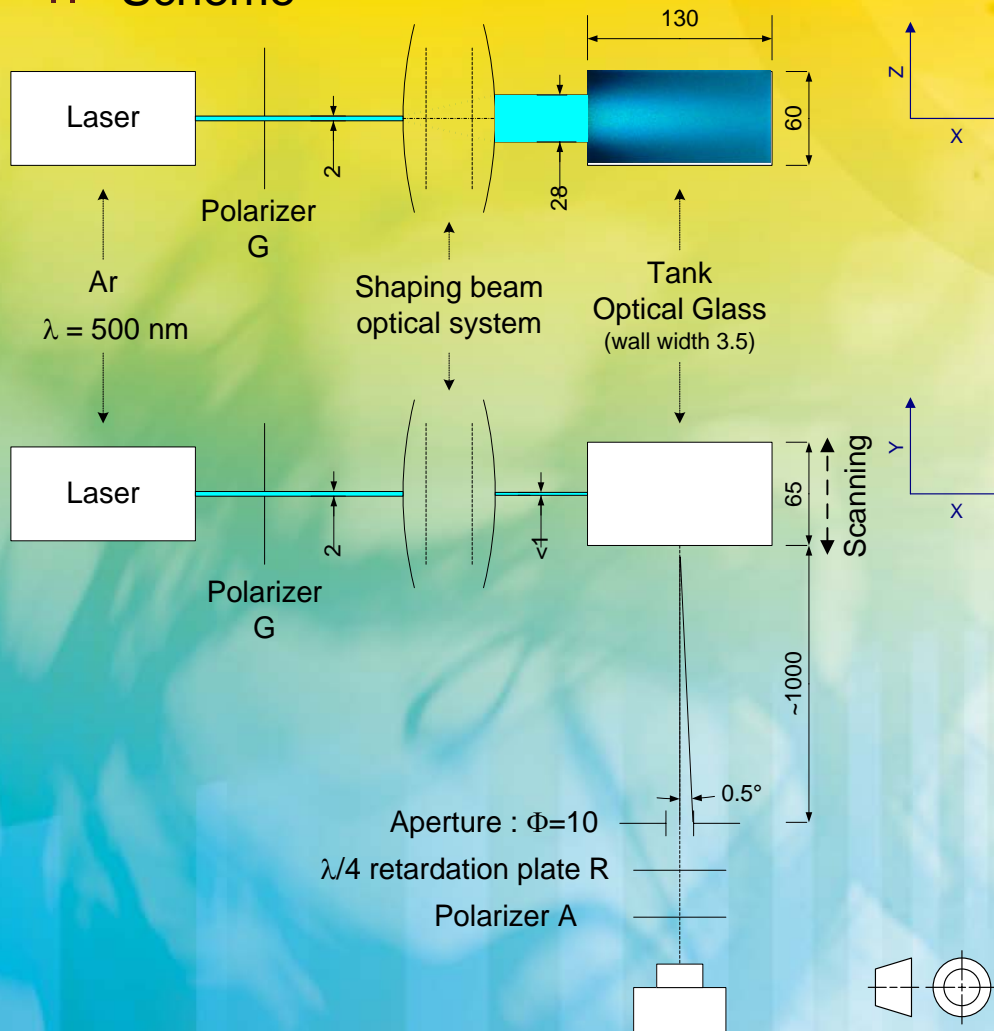
Polarizers

(generators and analyzers)

Extinction ratio $< 10^{-5}$

Experimental setup

✘ Scheme



✘ Principle

- For a given source, polarized by G, (I,Q,U,V) are measured with combinations of R and A

- $I = I_{0^\circ} + I_{90^\circ}$
- $Q = I_{0^\circ} - I_{90^\circ}$
- $U = I_{+45^\circ} - I_{-45^\circ}$
- $V = I_{\text{right}} - I_{\text{left}}$

- Then other quantities can be computed : Q/I, U/I

- Polarization degree

Total	Linear	Circular
$\frac{\sqrt{Q^2 + U^2 + V^2}}{I}$	$\frac{\sqrt{Q^2 + U^2}}{I}$	$\frac{V}{I}$

- 2D Mueller matrix

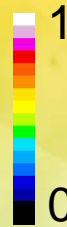
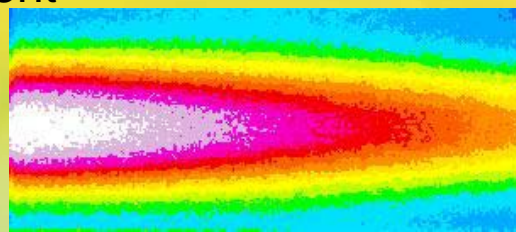
Some experimental results

source vertically polarized $(1,1,0,0)^t$

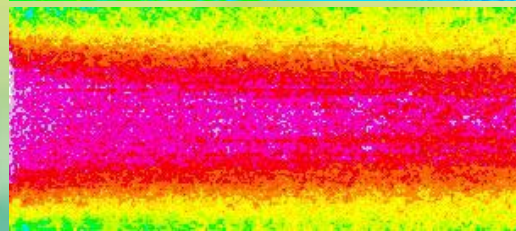
Size parameter $x = 0.8$
 Volume fraction $f_v = 0.01 \%$
 Scattering coefficient $\sigma = 20 \text{ m}^{-1}$

$x = 2.35$
 $f_v = 0.001 \%$
 $\sigma = 17 \text{ m}^{-1}$

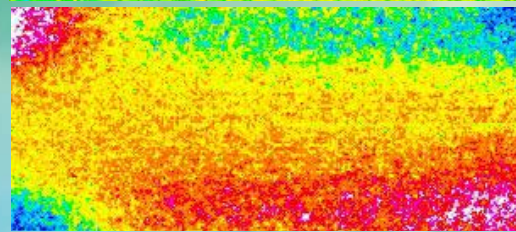
I/I_{\max}



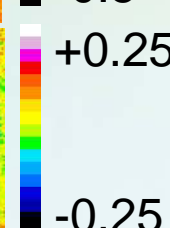
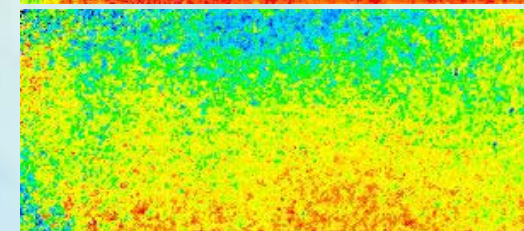
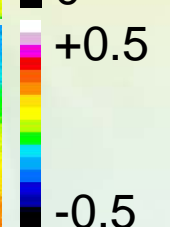
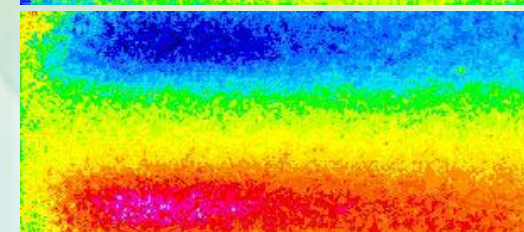
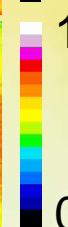
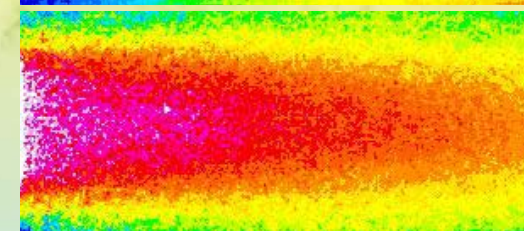
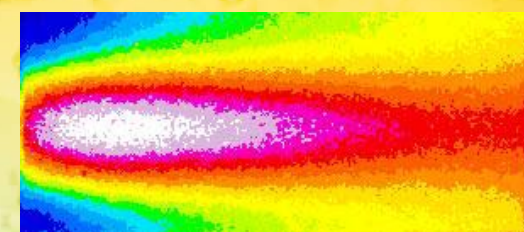
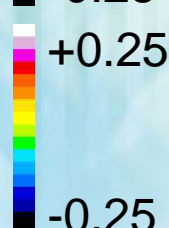
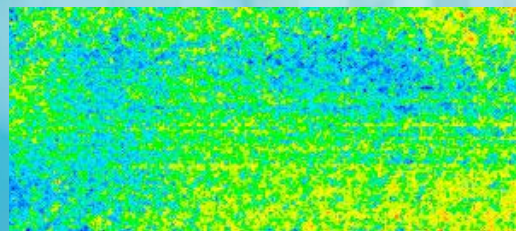
Q/I



U/I



V/I



Conclusion

- ✗ **A new model to generate polarization images in multiple scattering particle-laden media**
 - From the integral formulation of the VRTE
 - With efficient statistical principles for convergence optimization
- **Integral-Vector Monte Carlo Method**
- ✗ **Could potentially be applied to any 3D geometry and kind of particles** (provided that the issue of reflections at boundaries is addressed)
- ✗ Validated in the case of plane-parallel backscattering configurations
- ✗ **2D lateral Mueller matrix elements for a cubic tank filled with a uniform suspension of monodispersed particles**
 - → **Sensitivity of different Mueller matrix elements to particle size and morphology**

Expectation

✘ Further work

- Continuation of this analysis from physical and statistical points of view
- Extension to realistic situations such as systems undergoing an aggregation process
- Experimental investigations for comparison and application
- Step by step development of a parameter estimation methodology

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